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1 THERMODIFFUSION COEFFICIENTS OF WATER/ETHANOL MIXTURES FOR LOW WATER 2 MASS FRACTIONS

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8

9 Abstract

10 The difficulty of measuring the thermodiffusion
11 coefficients by optical properties of water-
12 ethanol binary mixtures of approximately 20 wt
13 % of water has been highlighted by several
14 authors in recent years. This is because the
15 concentration derivative of the refractive index
16 $(\partial n/\partial c)_{p,T}$ is near zero at this concentration.
17 For this reason, we measured the
18 thermodiffusion coefficients by means of density
19 analysis using the thermogravitational column
20 technique from 5 wt % to 50 wt % at 25°C. In
21 addition, we measured the thermophysical
22 properties such as density, dynamic viscosity,
23 thermal expansion and mass expansion.

24 **Keywords:** Thermodiffusion, binary mixtures,
25 Soret effect, thermophysical properties,
26 thermogravitational column.

27 1. Introduction

28 The presence of a temperature gradient in a
29 mixture creates a separation of the concentration
30 of the components in that mixture. This
31 phenomenon is known as the Ludwig-Soret
32 effect or the thermodiffusive effect. The Soret
33 coefficient is used to quantify this phenomenon.
34 In the case of binary mixtures, this coefficient
35 can be obtained by the relationship between the
36 concentration difference Δc , the temperature
37 difference ΔT and the initial concentration of
38 the reference component c_0 .

$$S_T = -\frac{1}{c_0(1-c_0)} \frac{\Delta c}{\Delta T} \quad (1)$$

39 In recent years, interest in mass transfer
40 mechanisms in multicomponent mixtures under a
41 temperature gradient has been increasing. This is

42 because of the relevance of this phenomenon in
43 different fields such as biology (Bahat and
44 Eisenbach 2006; Bonner and Sundelöf 1984;
45 Braun and Libchaber 2004), methods of
46 separation (Furry et al. 1939; Platten et al. 2003),
47 optimization of separation processes in
48 microdevices (Martin et al. 2011) and in the
49 petroleum industry (Ghorayeb et al. 2003;
50 Montel 1994).

51 Over time, several techniques have been
52 developed to analyse this phenomenon. Some of
53 the techniques are used in ground conditions: the
54 Optical Digital Interferometry (Mialdun and
55 Shevtsova 2011), the Optical Beam Deflection
56 (Gebhardt et al. 2013), the Thermal Diffusion
57 Forced Rayleigh Scattering (Wittko and Köhler
58 2003), the Thermogravitational Column (Bou-
59 Ali et al. 1998) and the Sliding Symmetric
60 Tubes (Larrañaga et al. 2014). In addition, the
61 Selectable Optical Diagnostic Instrument
62 technique (SODI) (Mialdun et al. 2013) is used
63 in microgravity conditions in the International
64 Space Station (ISS) in order to confirm the
65 ground condition results.

66 In this context, the DCMIX project was
67 established (Diffusion Coefficients
68 Measurements in Ternary Mixtures). The main
69 objective of this project is to study the
70 thermodiffusion effect in multicomponent
71 mixtures. The project is divided into different
72 phases to analyse different ternary mixtures. The
73 first one (DCMIX1), analysed mixtures
74 composed of hydrocarbons such as 1,2,3,4-
75 tetrahydronaphthalene (THN), dodecane (C12)
76 and isobutylbenzene (IBB). The results of one
77 ternary mixture of DCMIX1 were established as
78 a Benchmark (Bou-Ali et al. 2015). The second
79 phase DCMIX2, is measuring mixtures
80 composed of toluene, methanol and cyclohexane.
81 These particular mixtures, are characterized as
82 being critical because in some ranges of
83 concentrations there is an immiscibility gap and

84 the Soret coefficients are negative (Bou-Ali et al.
85 2000; Sechenyh et al. 2012; Story and Turner
86 1969; Wittko and Köhler 2006; Wittko and
87 Köhler 2005). The third phase, DCMIX3, is
88 focused on analysing aqueous mixtures, such as
89 water, ethanol and triethylene-glycol ternary
90 mixtures, and is the subject of this paper.

91 In the phases DCMIX1, DCMIX2 and
92 DCMIX3, binary mixtures and ternary mixtures
93 were analysed. In fact, in DCMIX1 Larrañaga et
94 al. determined new correlations to predict the
95 thermodiffusion (D_T) and Soret (S_T) coefficient
96 of ternary mixtures from binary mixtures
97 (Larrañaga et al. 2015). In addition, Sechenyh et
98 al. found expressions for the diffusion matrix of
99 a ternary mixture approaching the binary limits
100 (Sechenyh et al. 2015). In DCMIX2, the
101 thermodiffusion, molecular diffusion and Soret
102 coefficients of binary mixtures were analysed
103 (Lapeira et al. 2015)

104 Each of the abovementioned studies,
105 highlight the importance of analysing the
106 corresponding binary mixtures in each DCMIX
107 phase.

108 In this work, the analysis of water-ethanol
109 binary mixtures from DCMIX3 is presented.
110 These mixtures have been widely studied in
111 literature by different authors (Dutrieux et al.
112 2002; Kolodner et al. 1988; Mialdun and
113 Shevtsova 2008; Wiegand et al. 2007; Zhang et
114 al. 1996). In the water-ethanol system the
115 contrast factor $(\partial n/\partial c)_{p,T}$ is near zero at
116 approximately 20 wt % of water. For this reason,
117 the sensitivity is very low at these
118 concentrations, making it difficult to determine
119 the transport coefficients (S_T , D , D_T) accurately
120 by optical analysis (Kita et al. 2004; Königer et
121 al. 2009).

122 Due to this problem, we studied the behavior
123 of the thermodiffusion coefficient by means of
124 density analysis of water-ethanol binary mixtures
125 from 5.63 wt % to 50 wt % of water.

126 This article is organized as follows: in
127 Section 2, the determination of thermophysical
128 properties and the thermodiffusion coefficient
129 measured using the thermogravitational column
130 technique are explained. In Section 3, the results
131 of the thermophysical properties and the
132 thermodiffusion coefficients are shown. Finally,
133 Section 4 outlines the conclusions.

134 2. Experimental analysis

135 Determination of thermophysical properties

136 For the determination of the thermodiffusion
137 coefficient using thermogravitational column
138 technique, it is necessary to know some
139 thermophysical properties such as density,
140 viscosity, thermal expansion and mass
141 expansion.

142 The preparation of the sample was made with
143 the precision Gram VXi-310 balance with an
144 accuracy of $\pm 0.0001\text{g}$. The denser component
145 was added first, followed by the second
146 component. The density (ρ) was measured by the
147 Anton Paar DMA 5000 density meter with an
148 accuracy of $5 \times 10^{-3} \text{ kg/m}^3$. Thermal

149 expansion $\alpha = -\frac{1}{\rho} \left(\frac{\partial \rho}{\partial T} \right)_{c,p}$ and mass

150 expansion $\beta = \frac{1}{\rho} \left(\frac{\partial \rho}{\partial c} \right)_{T,p}$ coefficients were

151 also analysed using the same density meter. The
152 thermal expansion coefficient was determined by
153 analysing the density of one sample at different
154 temperatures. To measure the mass expansion,
155 we prepared 5 samples with a slight difference of
156 concentration and measured the density of each
157 concentration. Dynamic viscosity (μ) was
158 measured by two devices, the Anton Paar AMVn
159 falling ball microviscometer with an accuracy of
160 $\pm 0.002\text{s}$, and the manual Haake viscometer
161 with an accuracy of $\pm 0.2\text{s}$.

162 Determination of thermodiffusion coefficient

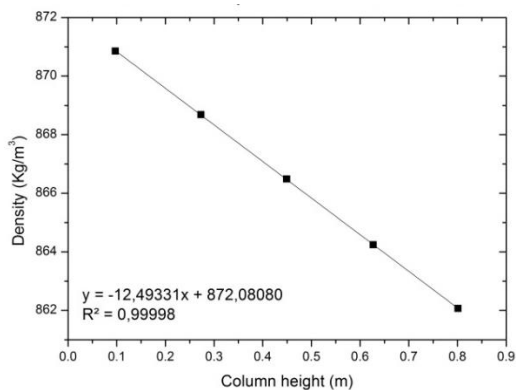
163 D_T

164 The thermodiffusion coefficient
165 measurements were performed using the
166 thermogravitational column technique (Bou-Ali
167 et al. 1998). In this technique, a horizontal
168 temperature gradient is applied which creates a
169 vertical separation of the concentration. When
170 the mixture reaches the stationary state, 5
171 samples are extracted at different heights of the
172 column and the density is measured to determine
173 the concentration distribution (2),

$$174 \Delta c = \frac{\partial c}{\partial \rho} \frac{\partial \rho}{\partial z} L_z \quad (2)$$

174 Where, $(\partial c/\partial \rho)_{p,T}$ is defined in a previous
175 calibration, $(\partial \rho/\partial z)_{p,T}$ is the variation of the

176 density along the length of the column (Fig. 1)
 177 and $L_z = (98.0 \pm 0.1)$ cm is the height of the long
 178 column.



179

180 **Fig. 1** Variation of density along the length of column
 181 of water-ethanol binary mixture at 31.25 wt % of
 182 water at steady state.

183 Finally, having measured the thermophysical
 184 properties the thermodiffusion coefficient was
 185 determined by the following equation (Bou-Ali
 186 et al. 1998),

$$D_T = -\frac{1}{504} \frac{L_x^4}{L_z} \frac{1}{c_0(1-c_0)} \frac{\alpha \cdot g \cdot \rho}{\mu} \Delta c \quad (4)$$

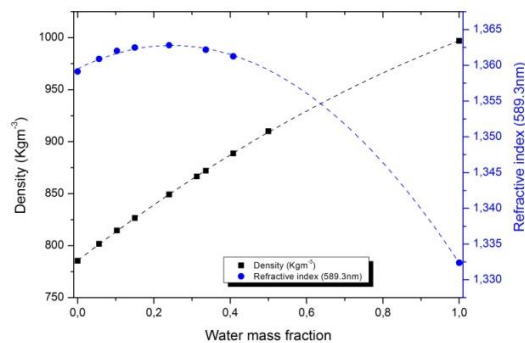
187 $L_x = (0.102 \pm 0.0005)$ cm is the gap of the
 188 column, c_0 is the concentration of the reference
 189 component and g is the gravity.

190 3. Results and discussion

191 There are works in the literature that mention
 192 the difficulty of measuring the thermodiffusion
 193 coefficients of water-ethanol binary mixtures by
 194 analysing the refractive index (Kita et al. 2004;
 195 Königer et al. 2009). When the water mass

196 fraction is approximately 20 wt %, the
 197 concentration derivative of the refractive index
 198 $(\partial n / \partial c)_{p,T}$ undergoes a sign change, and
 199 therefore the optical measurement sensitivity is
 200 reduced considerably and the errors bars
 201 increase.

202 Consequently, we measured the
 203 thermodiffusion coefficient by analysing the
 204 density. We deduced that the concentration
 205 derivative of the density is highly sensitive in
 206 this range of concentrations, see Fig. 2.



207

208 **Fig. 2** Density and refractive index ($\lambda=589.3$ nm) of
 209 water-ethanol binary mixtures as a function of water
 210 mass fraction at 25°C.

211 The thermodiffusion coefficients we obtained
 212 of water-ethanol binary mixtures are compared
 213 with the literature data in Fig. 3. There we can
 214 observe that there is quite good agreement
 215 between values near 50 wt % of water.
 216 Nevertheless, for 10.32 wt % of water, there is a
 217 marked difference between our results and those
 218 of (Königer et al. 2009). This difference might be
 219 because the measurements were based on
 220 different analysis methods: density analysis in
 221 the case of our research and refractive index
 222 analysis in the case of Königer

223

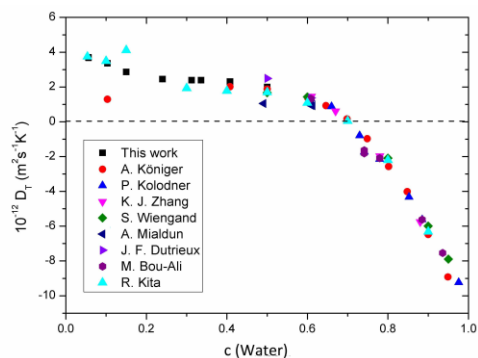
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Table 1 Thermodiffusion coefficients values of analysed binary mixtures at 25°C.

c	$(10^{-12}) D_T$ ($m^2 \cdot s^{-1} \cdot K^{-1}$)	ρ ($kg \cdot m^{-3}$)	β	$(10^{-3}) \alpha$ (K^{-1})	μ ($mPa \cdot s$)
0.0563	3.69 ± 0.17	801.815	0.350	1.087	1.184
0.1032	3.28 ± 0.13	814.734	0.324	1.077	1.305
0.15	2.94 ± 0.11	826.681	0.307	1.061	1.440
0.24	2.46 ± 0.08	849.208	0.287	1.025	1.673
0.3125	2.39 ± 0.08	866.574	0.273	0.983	1.852
0.336	2.28 ± 0.08	872.139	0.271	0.978	1.898
0.4079	2.31 ± 0.08	888.821	0.260	0.938	2.040
0.50	1.77 ± 0.07	910.085	0.245	0.885	2.134

226



227

228 **Fig. 3** Thermodiffusion coefficients (D_T) of
 229 water/ethanol as a function of mass fraction of water at
 230 25°C (This work) compared to A. König et al. at
 231 25°C (König et al. 2009), P. Kolodner et al. at 25°C
 232 (Kolodner et al. 1988), K. J. Zhang et al. at 25°C
 233 (Zhang et al. 1996), S. Wiegand et al. at 25°C
 234 (Wiegand et al. 2007), A. Mialdun et al. at 22.5°C
 235 (Mialdun and Shevtsova 2008), J. F. Dutrieux et al. at
 236 22.5°C (Dutrieux et al. 2002), M. M. Bou-Ali 25°C
 237 (Bou-Ali et al. 1999) and R. Kita at 22°C (Kita et al.,
 238 2004).

239 Table 1 shows the values of all D_T
 240 coefficients and thermophysical properties
 241 measured at 25°C. For this specific binary
 242 mixture at this range of concentrations, we think
 243 it is better to measure using the density analysis.

244 4. Conclusions

245 Using the thermogravitational column
 246 technique based on density analysis, the present
 247 study provides additional values of
 248 thermodiffusion coefficients of water-ethanol
 249 binary mixtures in the low water mass fraction
 250 range.

251 The results of this work at low water mass
 252 fractions have good agreement with the
 253 literature data except the 10.32 wt % of water.
 254 This might be because the literature values were
 255 based on refractive index analysis, while our
 256 results were based on density analysis. For this
 257 mixture, the sensitivity of the concentration
 258 derivative of the refractive index $(\partial n / \partial c)_{p,T}$ is
 259 very low thus the authors believe it is more
 260 accurate to analyse density instead of refractive
 261 index.

262 Until now, there has been a lack of reliable
 263 results in the range of concentrations for low
 264 water mass fractions. This research can serve as
 265 a base for future studies to determine the
 266 DCMIX3 ternary mixtures from binary
 267 mixtures.

268 Acknowledgements

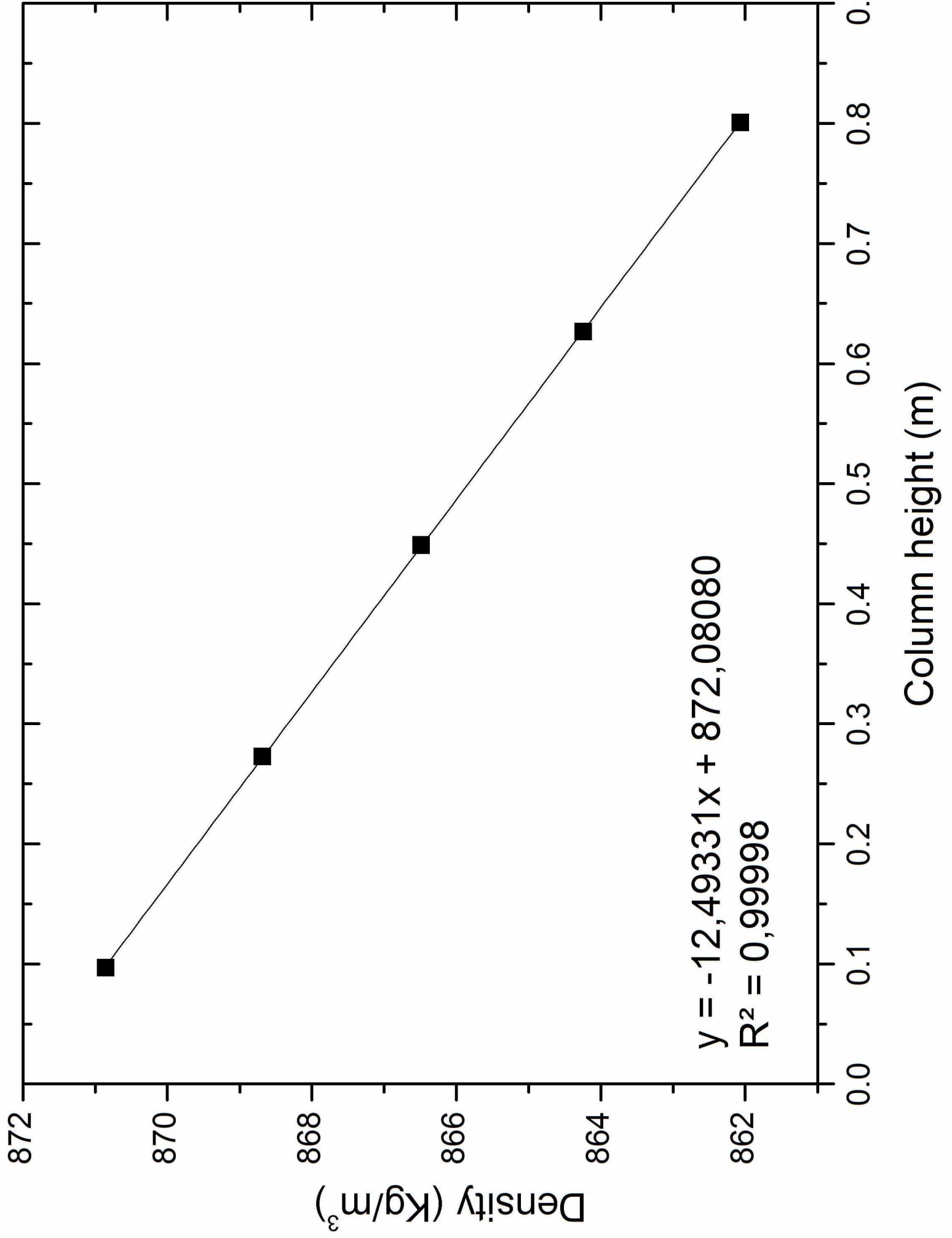
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 272 Basque Government, TERDISOMEZ (FIS2014-
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 275 Space Agency.

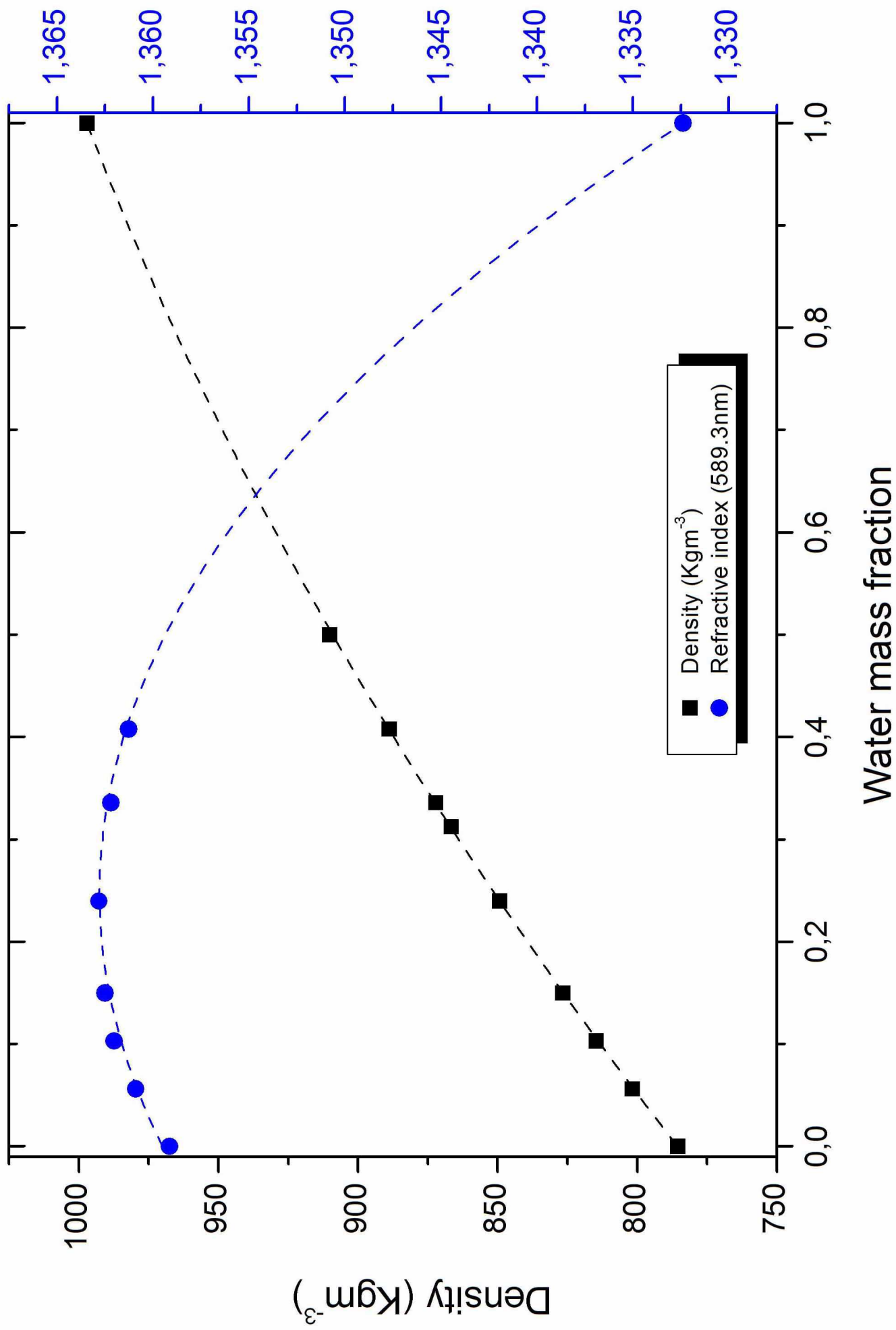
276 References

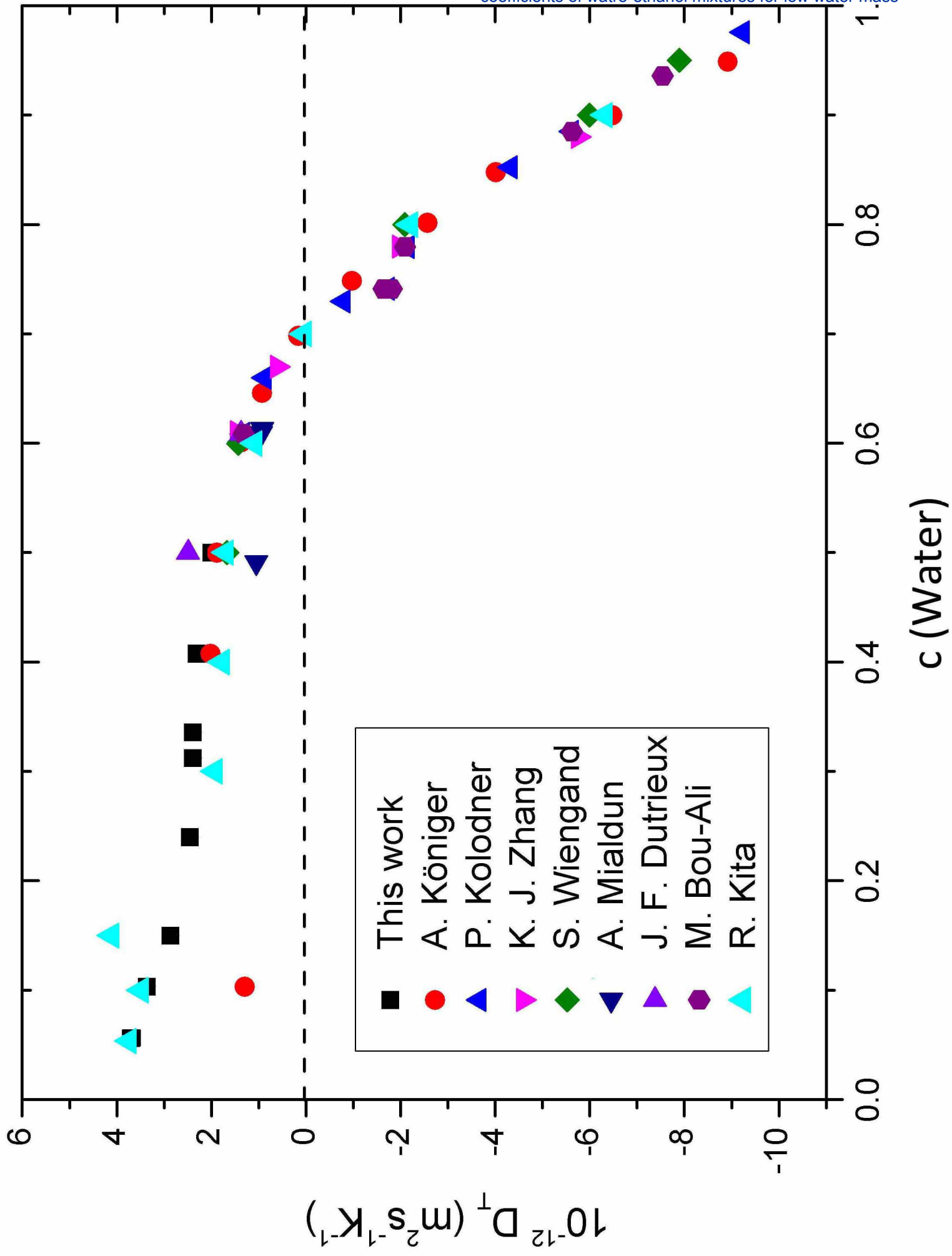
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figure1







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68 Measurements in Ternary Mixtures). The main
69 objective of this project is to study the
70 thermodiffusion effect in multicomponent
71 mixtures. The project is divided into different
72 phases to analyse different ternary mixtures. The
73 first one (DCMIX1), analysed mixtures
74 composed of hydrocarbons such as 1,2,3,4-
75 tetrahydronaphthalene (THN), dodecane (C12)
76 and isobutylbenzene (IBB). The results of one
77 ternary mixture of DCMIX1 were established as
78 a Benchmark (Bou-Ali et al. 2015). The second
79 phase DCMIX2, is measuring mixtures
80 composed of toluene, methanol and cyclohexane.
81 These particular mixtures, are characterized as
82 being critical because in some ranges of
83 concentrations there is an immiscibility gap and

84 the Soret coefficients are negative (Bou-Ali et al.
85 2000; Sechenyh et al. 2012; Story and Turner
86 1969; Wittko and Köhler 2006; Wittko and
87 Köhler 2005). The third phase, DCMIX3, is
88 focused on analysing aqueous mixtures, such as
89 water, ethanol and triethylene-glycol ternary
90 mixtures, and is the subject of this paper.

91 In the phases DCMIX1, DCMIX2 and
92 DCMIX3, binary mixtures and ternary mixtures
93 were analysed. In fact, in DCMIX1 Larrañaga et
94 al. determined new correlations to predict the
95 thermodiffusion (D_T) and Soret (S_T) coefficient
96 of ternary mixtures from binary mixtures
97 (Larrañaga et al. 2015). In addition, Sechenyh et
98 al. found expressions for the diffusion matrix of
99 a ternary mixture approaching the binary limits
100 (Sechenyh et al. 2015). In DCMIX2, the
101 thermodiffusion, molecular diffusion and Soret
102 coefficients of binary mixtures were analysed
103 (Lapeira et al. 2015)

104 Each of the abovementioned studies,
105 highlight the importance of analysing the
106 corresponding binary mixtures in each DCMIX
107 phase.

108 In this work, the analysis of water-ethanol
109 binary mixtures from DCMIX3 is presented.
110 These mixtures have been widely studied in
111 literature by different authors (Dutrieux et al.
112 2002; Kolodner et al. 1988; Mialdun and
113 Shevtsova 2008; Wiegand et al. 2007; Zhang et
114 al. 1996). In the water-ethanol system the
115 contrast factor $(\partial n/\partial c)_{p,T}$ is near zero at
116 approximately 20 wt % of water. For this reason,
117 the sensitivity is very low at these
118 concentrations, making it difficult to determine
119 the transport coefficients (S_T , D , D_T) accurately
120 by optical analysis (Kita et al. 2004; Königer et
121 al. 2009).

122 Due to this problem, we studied the behavior
123 of the thermodiffusion coefficient by means of
124 density analysis of water-ethanol binary mixtures
125 from 5.63 wt % to 50 wt % of water.

126 This article is organized as follows: in
127 Section 2, the determination of thermophysical
128 properties and the thermodiffusion coefficient
129 measured using the thermogravitational column
130 technique are explained. In Section 3, the results
131 of the thermophysical properties and the
132 thermodiffusion coefficients are shown. Finally,
133 Section 4 outlines the conclusions.

134 2. Experimental analysis

135 Determination of thermophysical properties

136 For the determination of the thermodiffusion
137 coefficient using thermogravitational column
138 technique, it is necessary to know some
139 thermophysical properties such as density,
140 viscosity, thermal expansion and mass
141 expansion.

142 The preparation of the sample was made with
143 the precision Gram VXi-310 balance with an
144 accuracy of $\pm 0.0001\text{g}$. The denser component
145 was added first, followed by the second
146 component. The density (ρ) was measured by the
147 Anton Paar DMA 5000 density meter with an
148 accuracy of $5 \times 10^{-3} \text{ kg/m}^3$. Thermal

149 expansion $\alpha = -\frac{1}{\rho} \left(\frac{\partial \rho}{\partial T} \right)_{c,p}$ and mass

150 expansion $\beta = \frac{1}{\rho} \left(\frac{\partial \rho}{\partial c} \right)_{T,p}$ coefficients were

151 also analysed using the same density meter. The
152 thermal expansion coefficient was determined by
153 analysing the density of one sample at different
154 temperatures. To measure the mass expansion,
155 we prepared 5 samples with a slight difference of
156 concentration and measured the density of each
157 concentration. Dynamic viscosity (μ) was
158 measured by two devices, the Anton Paar AMVn
159 falling ball microviscometer with an accuracy of
160 $\pm 0.002\text{s}$, and the manual Haake viscometer
161 with an accuracy of $\pm 0.2\text{s}$.

162 Determination of thermodiffusion coefficient

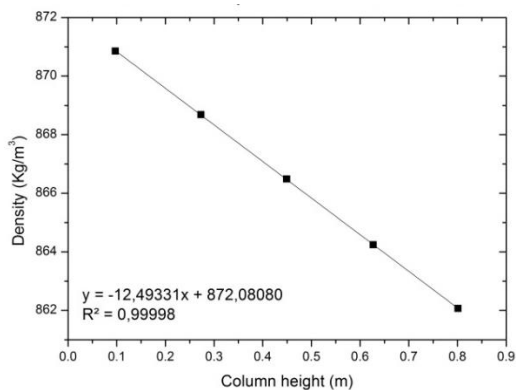
163 D_T

164 The thermodiffusion coefficient
165 measurements were performed using the
166 thermogravitational column technique (Bou-Ali
167 et al. 1998). In this technique, a horizontal
168 temperature gradient is applied which creates a
169 vertical separation of the concentration. When
170 the mixture reaches the stationary state, 5
171 samples are extracted at different heights of the
172 column and the density is measured to determine
173 the concentration distribution (2),

$$174 \Delta c = \frac{\partial c}{\partial \rho} \frac{\partial \rho}{\partial z} L_z \quad (2)$$

174 Where, $(\partial c/\partial \rho)_{p,T}$ is defined in a previous
175 calibration, $(\partial \rho/\partial z)_{p,T}$ is the variation of the

176 density along the length of the column (Fig. 1)
 177 and $L_z = (98.0 \pm 0.1)$ cm is the height of the long
 178 column.



179

180 **Fig. 1** Variation of density along the length of column
 181 of water-ethanol binary mixture at 31.25 wt % of
 182 water at steady state.

183 Finally, having measured the thermophysical
 184 properties the thermodiffusion coefficient was
 185 determined by the following equation (Bou-Ali
 186 et al. 1998),

$$D_T = -\frac{1}{504} \frac{L_x^4}{L_z} \frac{1}{c_0(1-c_0)} \frac{\alpha \cdot g \cdot \rho}{\mu} \Delta c \quad (4)$$

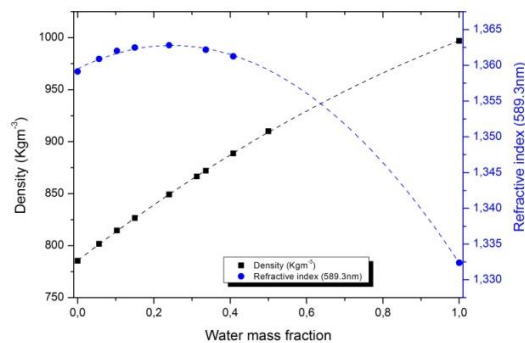
187 $L_x = (0.102 \pm 0.0005)$ cm is the gap of the
 188 column, c_0 is the concentration of the reference
 189 component and g is the gravity.

190 3. Results and discussion

191 There are works in the literature that mention
 192 the difficulty of measuring the thermodiffusion
 193 coefficients of water-ethanol binary mixtures by
 194 analysing the refractive index (Kita et al. 2004;
 195 Königer et al. 2009). When the water mass

196 fraction is approximately 20 wt %, the
 197 concentration derivative of the refractive index
 198 $(\partial n / \partial c)_{p,T}$ undergoes a sign change, and
 199 therefore the optical measurement sensitivity is
 200 reduced considerably and the errors bars
 201 increase.

202 Consequently, we measured the
 203 thermodiffusion coefficient by analysing the
 204 density. We deduced that the concentration
 205 derivative of the density is highly sensitive in
 206 this range of concentrations, see Fig. 2.



207

208 **Fig. 2** Density and refractive index ($\lambda=589.3$ nm) of
 209 water-ethanol binary mixtures as a function of water
 210 mass fraction at 25°C.

211 The thermodiffusion coefficients we obtained
 212 of water-ethanol binary mixtures are compared
 213 with the literature data in Fig. 3. There we can
 214 observe that there is quite good agreement
 215 between values near 50 wt % of water.
 216 Nevertheless, for 10.32 wt % of water, there is a
 217 marked difference between our results and those
 218 of (Königer et al. 2009). This difference might be
 219 because the measurements were based on
 220 different analysis methods: density analysis in
 221 the case of our research and refractive index
 222 analysis in the case of Königer

223

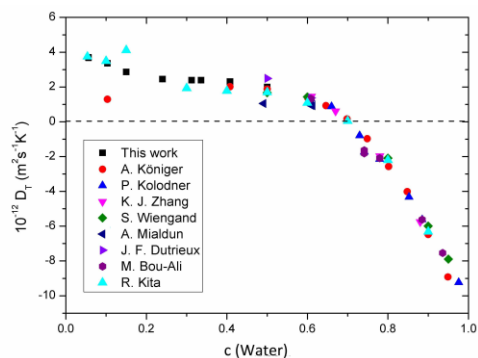
224

225

Table 1 Thermodiffusion coefficients values of analysed binary mixtures at 25°C.

c	$(10^{-12}) D_T$ ($m^2 \cdot s^{-1} \cdot K^{-1}$)	ρ ($kg \cdot m^{-3}$)	β	$(10^{-3}) \alpha$ (K^{-1})	μ ($mPa \cdot s$)
0.0563	3.69 ± 0.17	801.815	0.350	1.087	1.184
0.1032	3.28 ± 0.13	814.734	0.324	1.077	1.305
0.15	2.94 ± 0.11	826.681	0.307	1.061	1.440
0.24	2.46 ± 0.08	849.208	0.287	1.025	1.673
0.3125	2.39 ± 0.08	866.574	0.273	0.983	1.852
0.336	2.28 ± 0.08	872.139	0.271	0.978	1.898
0.4079	2.31 ± 0.08	888.821	0.260	0.938	2.040
0.50	1.77 ± 0.07	910.085	0.245	0.885	2.134

226



227

228 **Fig. 3** Thermodiffusion coefficients (D_T) of
 229 water/ethanol as a function of mass fraction of water at
 230 25°C (This work) compared to A. König et al. at
 231 25°C (König et al. 2009), P. Kolodner et al. at 25°C
 232 (Kolodner et al. 1988), K. J. Zhang et al. at 25°C
 233 (Zhang et al. 1996), S. Wiegand et al. at 25°C
 234 (Wiegand et al. 2007), A. Mialdun et al. at 22.5°C
 235 (Mialdun and Shevtsova 2008), J. F. Dutrieux et al. at
 236 22.5°C (Dutrieux et al. 2002), M. M. Bou-Ali 25°C
 237 (Bou-Ali et al. 1999) and R. Kita at 22°C (Kita et al.,
 238 2004).

239 Table 1 shows the values of all D_T
 240 coefficients and thermophysical properties
 241 measured at 25°C. For this specific binary
 242 mixture at this range of concentrations, we think
 243 it is better to measure using the density analysis.

244 4. Conclusions

245 Using the thermogravitational column
 246 technique based on density analysis, the present
 247 study provides additional values of
 248 thermodiffusion coefficients of water-ethanol
 249 binary mixtures in the low water mass fraction
 250 range.

251 The results of this work at low water mass
 252 fractions have good agreement with the
 253 literature data except the 10.32 wt % of water.
 254 This might be because the literature values were
 255 based on refractive index analysis, while our
 256 results were based on density analysis. For this
 257 mixture, the sensitivity of the concentration
 258 derivative of the refractive index $(\partial n / \partial c)_{p,T}$ is
 259 very low thus the authors believe it is more
 260 accurate to analyse density instead of refractive
 261 index.

262 Until now, there has been a lack of reliable
 263 results in the range of concentrations for low
 264 water mass fractions. This research can serve as
 265 a base for future studies to determine the
 266 DCMIX3 ternary mixtures from binary
 267 mixtures.

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